

Overview FOD methods

Update on decay method for slotted FOD

WPC1903 September 2019

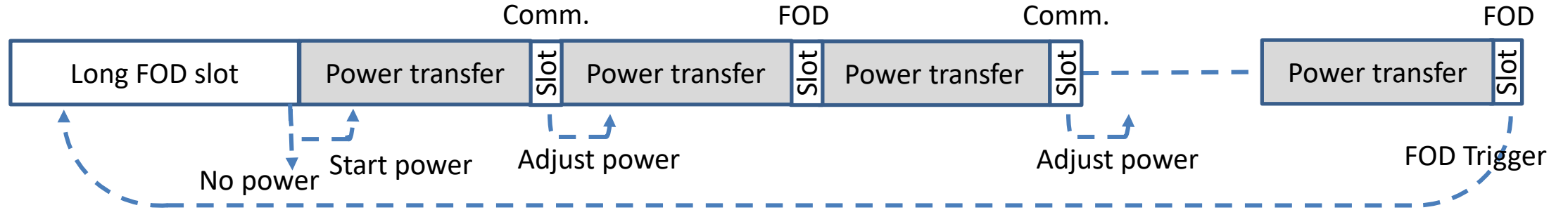
FOD methods for Qi

| Version | Impedance measurement | <i>Advantages</i> <i>Disadvantages</i> | Power measurement | <i>Advantages</i> <i>Disadvantages</i> |
|------------|---|--|--|--|
| | Before power transfer Disconnected load | <i>Not during power transfer</i> <i>Excludes uncertainty of load</i> <i>Indirect relation to FO power</i> | During power transfer Connected load | <i>During power transfer</i> <i>Uncertainty of load</i> <i>Direct relation to FO power</i> |
| V1.0 | | | Rectified power | <i>Simple implementation</i> <i>Uncertainty of internal losses not considered</i> |
| V1.1 | | | Power loss $P_{loss} = P_{Tx} - P_{Rx}$ Rx → Tx: received power | <i>Internal power losses included</i> <i>Synced measurements</i> <i>Insufficient resolution for >5W</i> |
| V1.2 | Q factor Rx → Tx: ref Q factor | <i>Tx design differences</i> <i>Influence of Rx distance</i> | Calibrated power loss Rx → Tx: received power + type Calibration at start of power transfer | <i>Relative values → better resolution</i> <i>Calibration depends on FO absence before power transfer</i> |
| V1.3 draft | Q factor + F resonance Rx → Tx: ref Q factor Rx → Tx: ref f factor | <i>Combined info</i> <i>Enhanced protocol support</i> <i>EFOD: Porting to reference</i> <i>Influence of Rx distance</i> | Calibrated power loss multipoint at start and during power to include multiple loads | <i>Better resolution over whole power range</i> <i>Increased risk: calibration while FO is present</i> |

Take-aways from Qi FOD methods

- Q factor method before power transfer
 - more accurate than power loss
 - uncertainty of load is excluded
- Power loss method during power transfer
 - Uncertainty reduction by calibration
 - Dependent on FOD before power transfer
- Protocol enhancements in v1.3 draft
 - Reference resonance shift in addition to Reference Q factor
 - Multipoint calibration for power loss
 - Protocol enhancements Re-start at FOD
- Further improvements of pre-power methods addressed by EFOD taskforce
 - Porting of measurements by Tx design to reference Tx
 - Combination Q-factor and resonance shift
 - Currently not described in draft v1.3
- Insufficient resolution / no prove for safe power > 15W
- No compensation for different positioning of Rx (XY + Z)

Slotted FOD (2017, May 5)



- Long FOD & Comm. slot (load disconnected)
 - Prepare for FOD (Rx communicates boundaries)
 - Find optimal parameters for FOD measurement and store them
 - Apply stored parameters and take multiple measurements
 - Compare measurements to boundaries
 - Determine safe maximum field (which could be zero)
- Power transfer (load connected) – e.g. 100ms
 - Apply safe power signal
- Short FOD Slot (load disconnected) – e.g. 1ms
 - Apply stored parameters for fast FOD
 - At FOD trigger (e.g. by exceeding threshold multiple times) → Long FOD slot
 - Note: position change of device may also cause FOD trigger
- Short Comm. slot (load disconnected) – e.g. 1ms
 - Communicate control information to adjust power
- Flexible use of short slots, e.g.
 - Alternating FOD, Communication
 - Combined FOD + communication in single slot

Medium power proposals for FOD

All proposals with disconnected load to exclude uncertainty of load

| Method | PTx only before Rx placement | PTx+PRx Long slot ~100ms “Before” power transfer | <i>Advantages</i> <i>Disadvantages</i> | PTx+PRx Short slot <1ms “During” power transfer | <i>Advantages</i> <i>Disadvantages</i> |
|--|--|--|---|--|--|
| | No influence of Rx | Absolute measurements considering influence of Rx | <i>High accuracy</i> <i>Multiple parameters</i> <i>Long interruption of power transfer</i> | Relative measurements in given constellation | <i>Calibration depends on FO absence in long slot</i> <i>Short interruption of power transfer</i> |
| Q factor frequency domain | Expected Q factor of Tx | Q curve Rx→Tx: frequency dependent Q curve Calibration to references | <i>Accurate method</i> <i>Compensation for distance</i> <i>Allows variation Tx and Rx coils</i> <i>Indirect relation to FO power</i> | Q factor for single frequency determined during long slot | <i>Interruption 1ms</i> <i>Need to swap to predetermined frequency</i> |
| Decay time domain | <i>Not proposed yet</i> | Decay curve <i>Not proposed yet</i> | <i>Allows for fixed frequency design</i> <i>TBD</i> | ΔDecay Multipoint calibration (new) | <i>Interruption 100us</i> <i>No predetermined setting</i> |
| Power loss | <i>Expected power loss in Tx</i> | Power loss (disconnected load) Rx→Tx: $R_{friendly} + U_{Rxcoil}$ | <i>Direct relation to FO power</i> <i>Compensation for distance / offset</i> <i>Complex compensation</i> | ΔPower loss (disconnected load) for single setting determined during long slot | <i>Interruption 1ms</i> <i>Need to swap to predetermined setting</i> |

From Bosch proposals

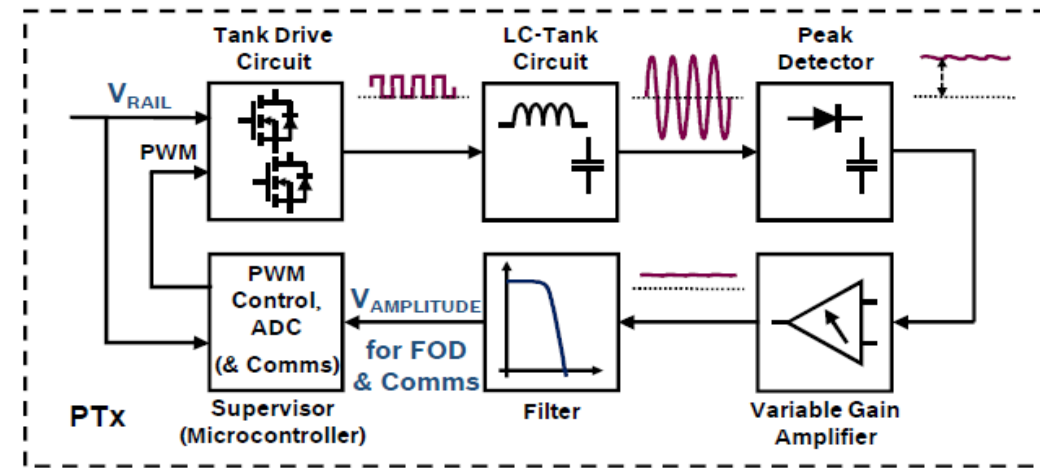
FOD via Q-Factor Measurement at Resonant Frequency

At the transmitter (PTx), while power is **not** being transferred...

- Q-Factor (k_Q) is calculated as the ratio of the peak tank circuit voltage ($V_{AMPLITUDE}$) versus the the exciting voltage (V_{RAIL}):

$$k_Q = V_{AMPLITUDE} / V_{RAIL} \quad \dots(1)$$

- A maximum k_Q found within the expected frequency range together with the corresponding frequency, represent the resonant frequency parameters (k_{Q_RES} , F_{RES}) of the system.



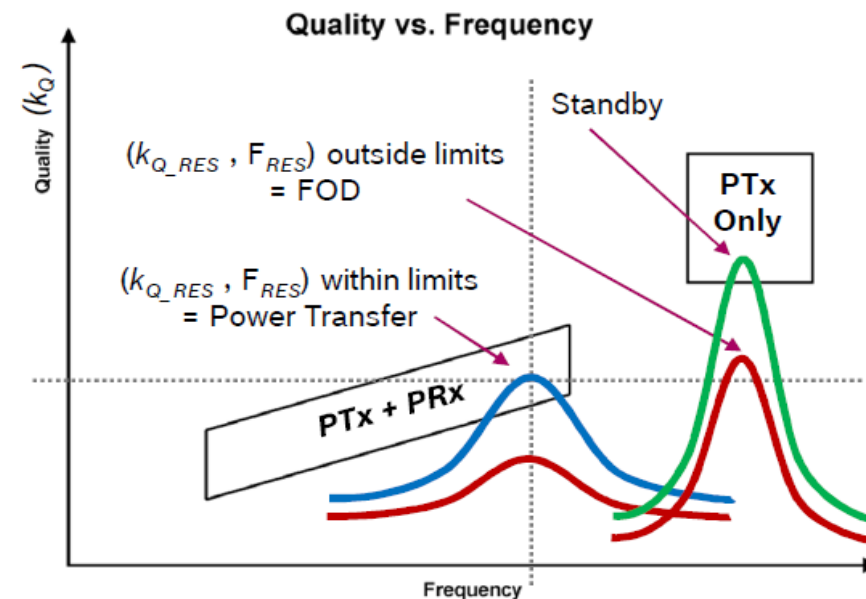
From Bosch proposals

Quality and Frequency Limits - Look-up-Table comparison

- The measured resonance frequency parameters (k_{Q_RES} , F_{RES}) are compared to predefined limits for a given transmitter and also for combinations of transmitter+receiver
- Changes in k_{Q_RES} and F_{RES} over time indicate changes in the system:
 - FO present
 - Change in PRx vs PTx alignment (Z, or in X or Y)

If (k_{Q_RES} , F_{RES}) are ..

- Within PTx+PRx region limits → Power transfer can proceed (preceded by PRx – PTx communications)
- Within PTx region limits → Standby
- Outside limits → FOD is present



From joint Philips Bosch proposal @WPC 1901

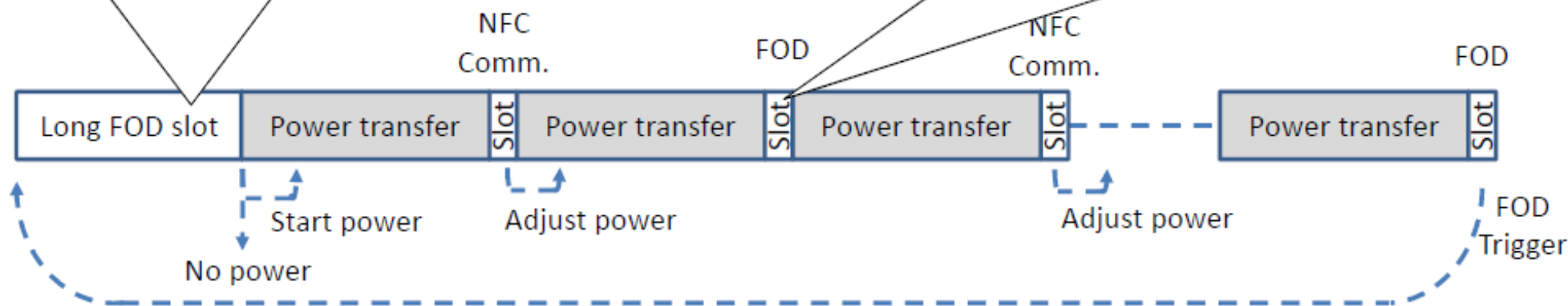
Q-Factor FOD method in long slot / short slot scheme

Long FOD slot (load disconnected)

- Prepare for FOD (Rx communicates reference values)
- Find PTx resonant frequency (F_{RES}) and measure K_{Q_RES} , V_{peak_RES}
- Compare measurements to boundaries
- Store F_{RES} , V_{peak_RES} and inverter settings (voltage /duty cycle) for use during short power slots.

Short FOD slot (load disconnected)

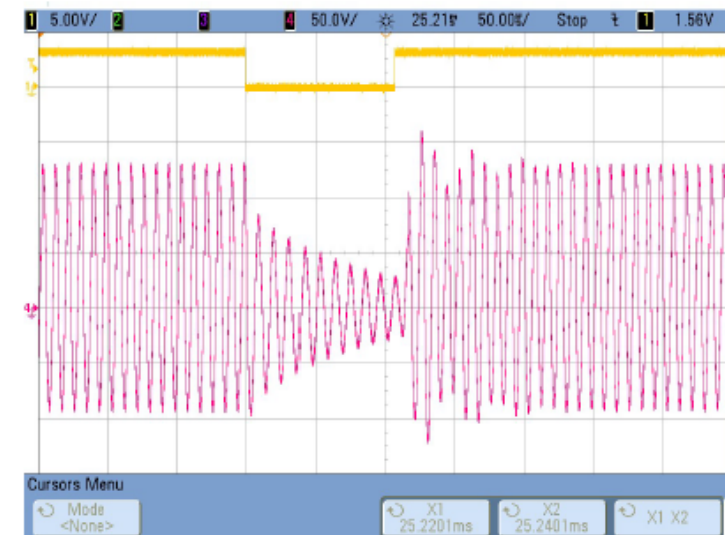
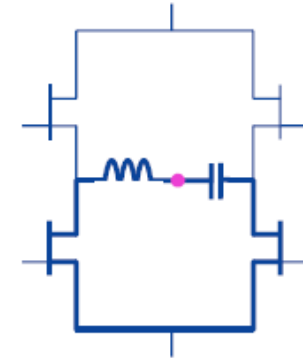
- Apply stored parameters for fast FOD (F_{RES} , inverter voltage / duty cycle)
- Measure V_{peak} and compare with reference level from long slot
- At FOD trigger => Long FOD slot (FOD triggers when V_{peak} deviates $> 3\%$ from V_{peak_RES})



From Philips proposal @WPC 1902

Short slot approach (1/2)

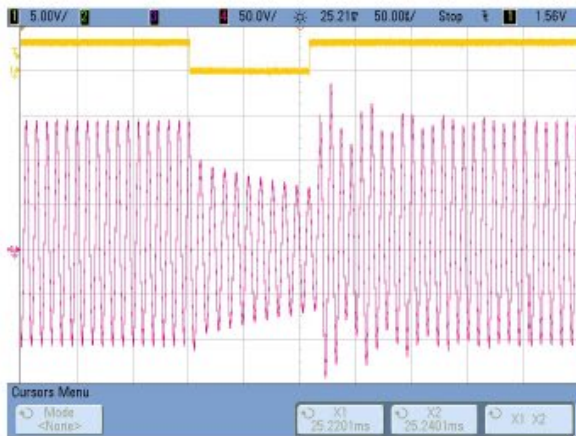
- Short-circuit the resonant tank with the low-side H-bridge switches
- Signal will decay under the influence of:
 - PTx system resistance
 - Friendly metal
 - Foreign objects
- Load basically 'disconnected' because the rectifier in the PRx is no longer conducting
 - Valid when: DC bus voltage > voltage induced in PRx coil
 - No influence of PRx coil current on PTx signal decay
- Short FOD slot duration: 100 μ s during initial testing



From Philips proposal @WPC 1902

Short slot approach (2/2)

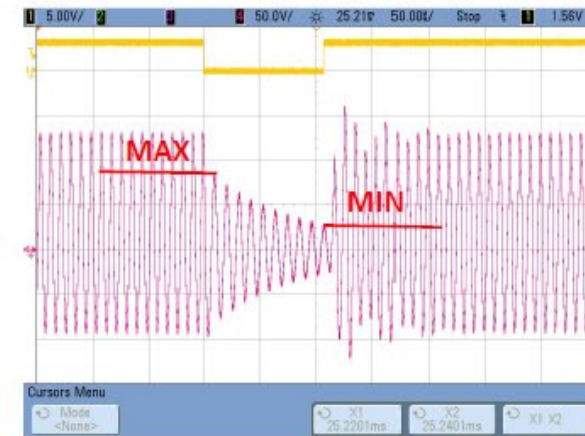
- Measure the decay of PTx resonant tank voltage during a short FOD slot
- Improve accuracy by averaging over multiple short FOD slots
- Compare average decay against threshold



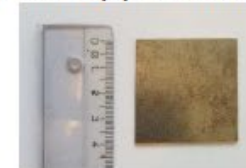
No FO



Small coin as FO



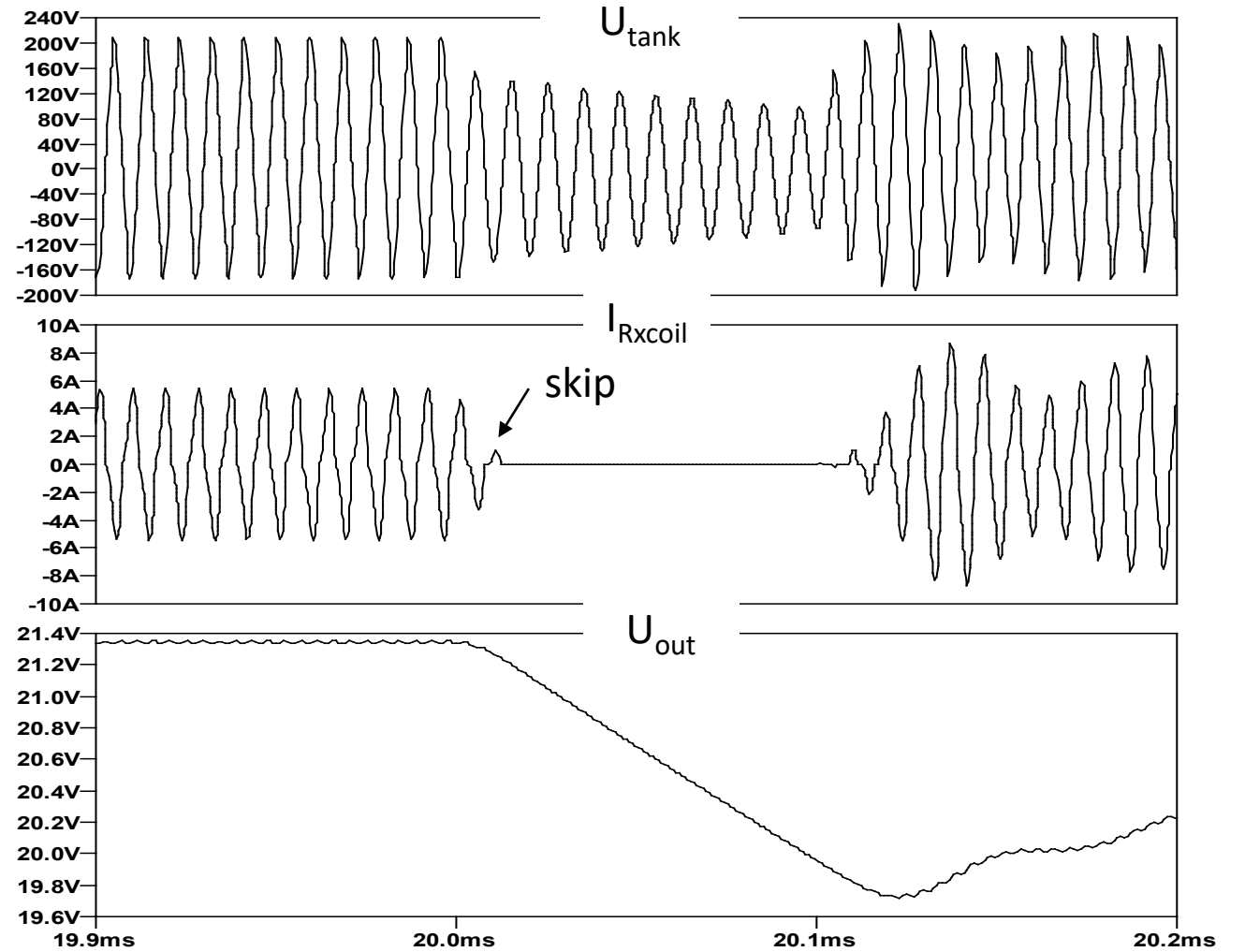
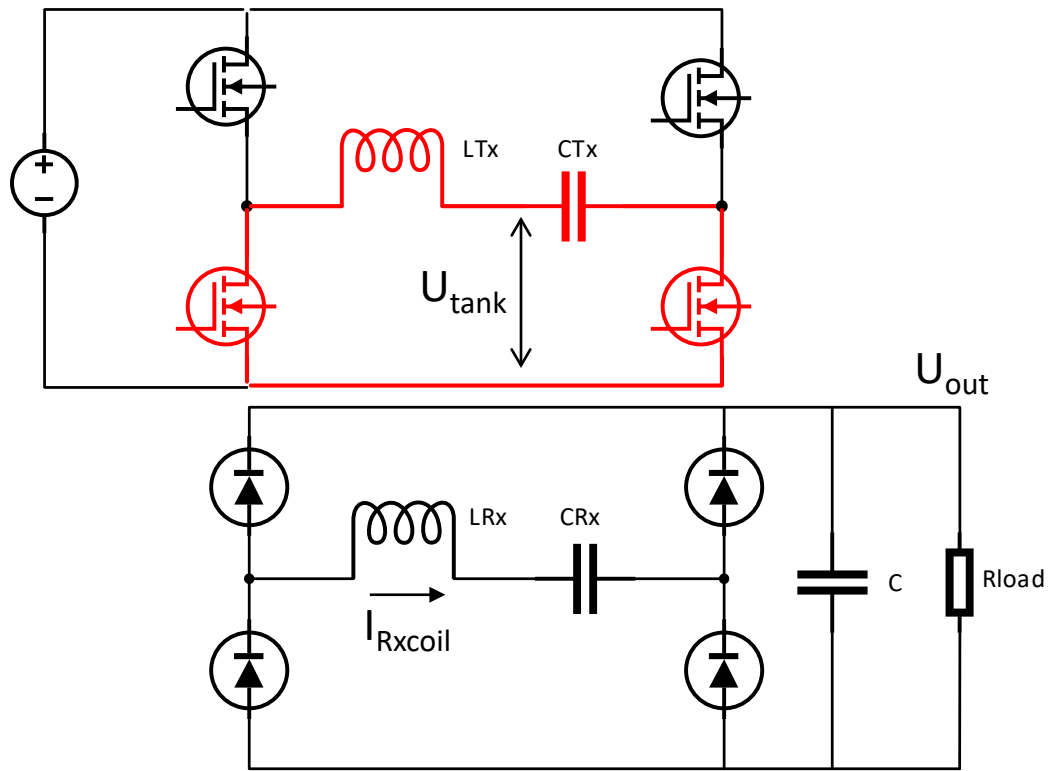
Piece of copper sheet as FO



Update Decay method

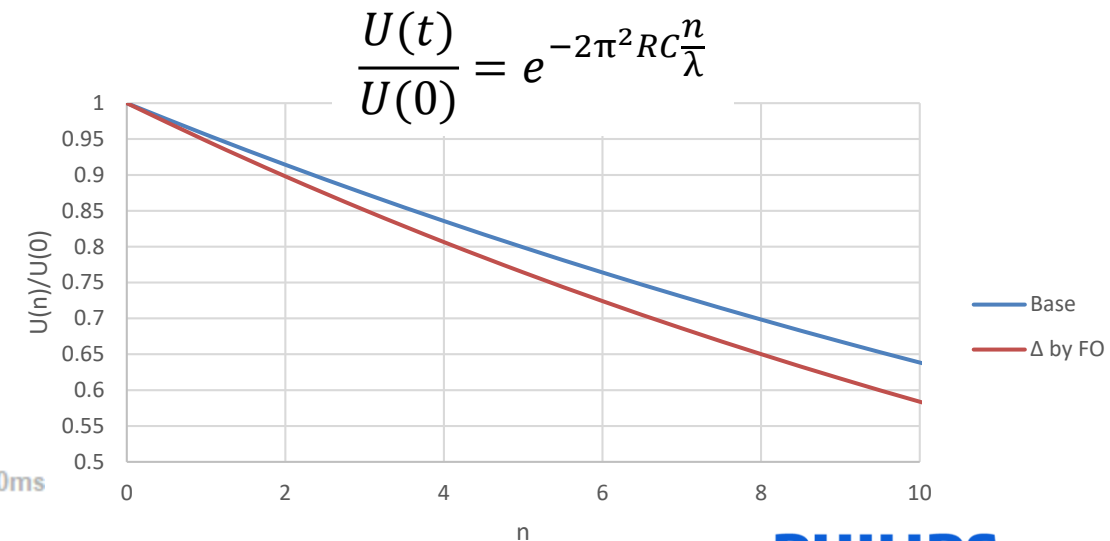
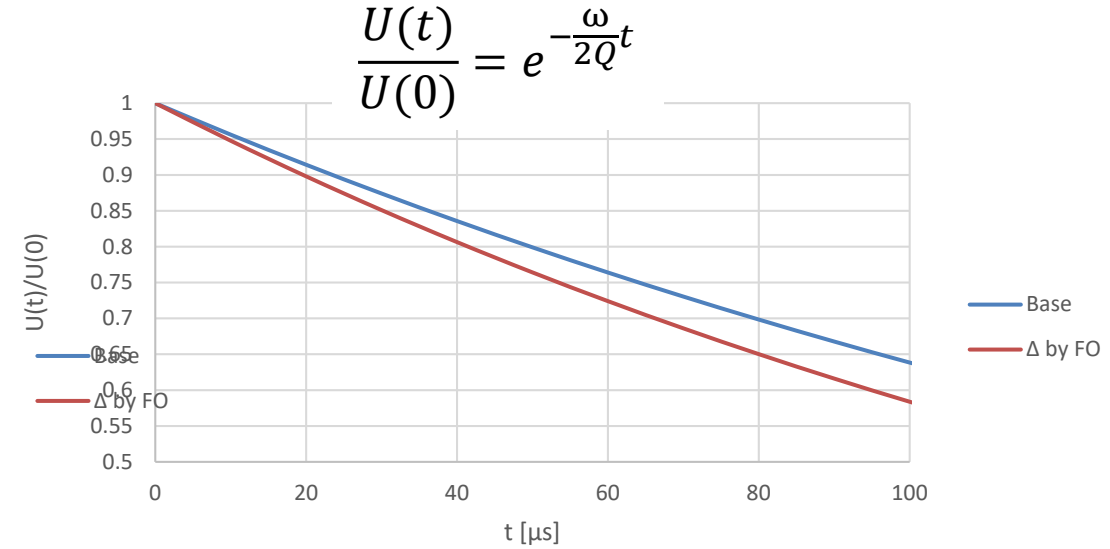
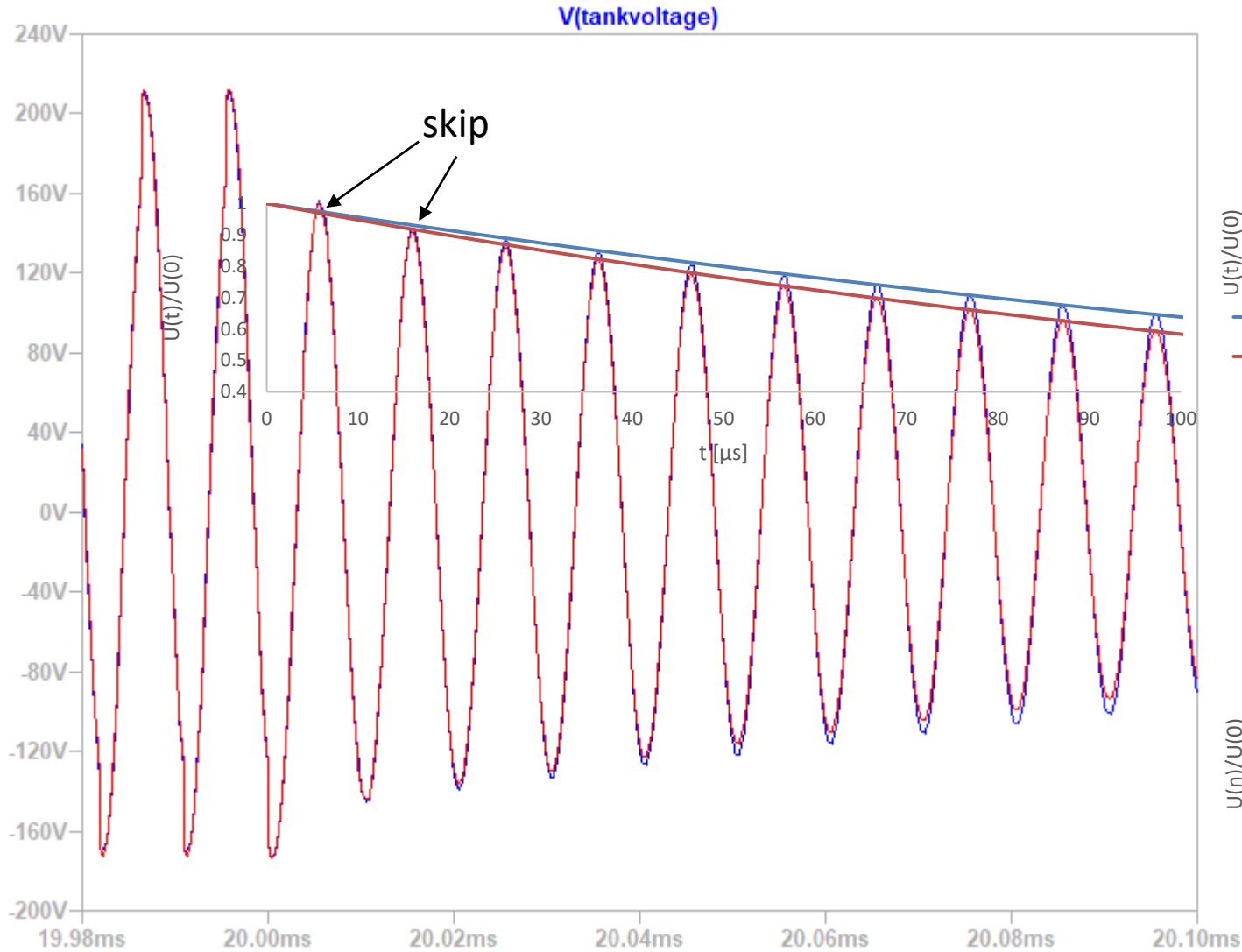
- Ensure to measure at time that load is disconnected
 - Start decay measurement after 2 cycles
- Calibration
 - Decay depends on operating point
 - Apply (auto)calibration for multiple operating points
- Calculations
 - Safe operation by limiting coil current
 - Related to ESR offset (ΔR) of resonance tank
 - to limit potential power dissipation in FOD

Decay method

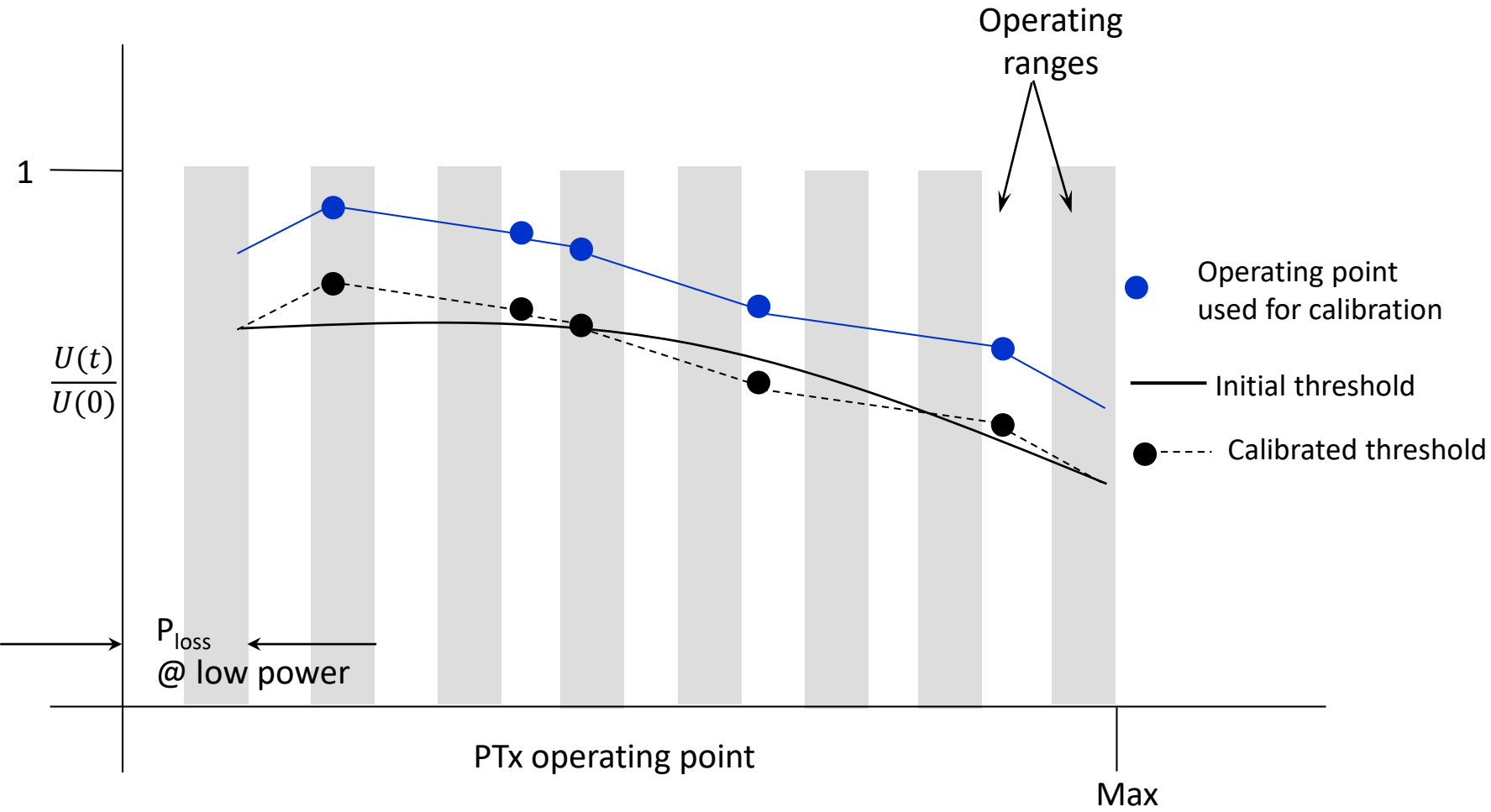


Δ Decay caused by FO

Example: $L=28\mu\text{H}$, $f=100\text{kHz}$, $R=250\text{m}\Omega$, $\Delta R (R_{FO})=50\text{m}\Omega$, $Q=70$, $\Delta Q=11.7$



Multipoint calibration for Δ decay



Trigger for calibration at:

- start of power transfer
- change of operating range

- FOD trigger if
Measured $\frac{U(t)}{U(0)} < \text{Threshold}$

Calculations

| | | | |
|------------------------------------|--|-----------|--|
| Decay: | $\frac{U(t)}{U(0)} = e^{-\frac{\omega}{2Q}t}$ | $U(0)$ | Resonance tank Voltage at start of decay measurement |
| | | $U(t)$ | Resonance tank Voltage at time t |
| | | t | time from start of decay measurement |
| with $Q = \frac{1}{\omega RC}$ | $\frac{U(t)}{U(0)} = e^{-\frac{\omega^2 RC}{2}t}$ | Q | Q factor |
| | | f | resonance frequency $f = \omega/2\pi$ |
| | | λ | wavelength = period of a resonance cycle $\lambda = 2\pi/\omega$ |
| Over n cycles: $t = n\lambda$ | $\frac{U(t)}{U(0)} = e^{-\frac{\pi}{Q}n}$ | n | number of wavelengths for decay measurement |
| | | C | capacitor of resonance circuit |
| with $Q = \frac{\lambda}{2\pi RC}$ | $\frac{U(t)}{U(0)} = e^{-2\pi^2 RC \frac{n}{\lambda}}$ | R | ESR of resonance circuit |
| | | R_{FO} | ΔR caused by FO |
| | | I | rms current in Tx coil |

For fixed C , R can be calculated:

With measured f and Q :

$$R = \frac{1}{2\pi f Q C}$$

With configured n and measured λ : $R = \frac{-\lambda}{2\pi^2 n C} \ln \left(\frac{U(t)}{U(0)} \right)$

Safe operation:

Limit primary coil current by estimation of P_{FO}

$$P_{FO} = I^2 R_{FO} = I^2 \Delta R \rightarrow I^2 \leq \frac{P_{FOmax}}{\Delta R}$$

Slotted FOD for Δ decay in short slots

Long Slot

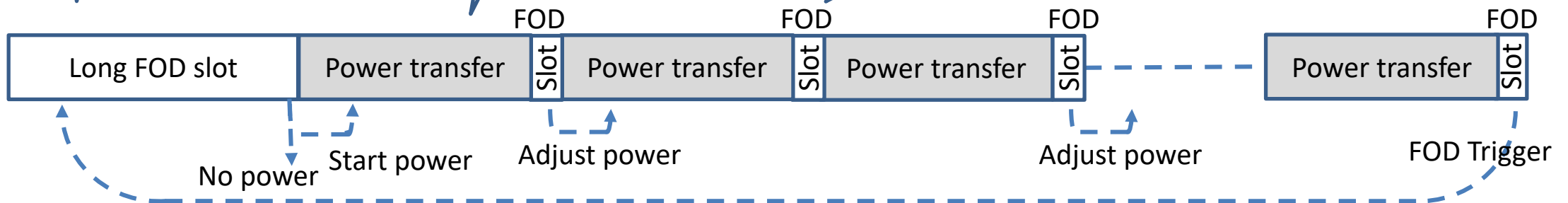
- E.g. Q curve method
- Determine safe maximum field
 - $I^2 \leq \frac{P_{FODmax}}{\Delta R}$

Power transfer

- Apply safe maximum field

Short Slot, decay method

- Wait for 2 cycles
- Measure decay: $\frac{U(t)}{U(0)}$ over time = t or $n\lambda$
- Average decay (e.g. over 75 slots in 2 seconds)
- FOD trigger: Average decay-value < threshold



Conclusions

- Proposals for medium power
 - Learnings from Qi
 - Measure at disconnected load
 - Calibrate power loss
 - Add more parameters
 - Accurate FOD in long slot
 - Multiple parameters: e.g. Q , f , U_{Rxcoil} , etc.
 - Compensate for different offset and distance positions
 - Calibration routines to compensate for design variations
 - FOD in short slot
 - Predefined settings, e.g. frequency and/or
 - Calibrated relative measurements, e.g. Δ decay
- Multiple methods enables
 - Design freedom
 - Increased reliability
 - Smart combinations, e.g.
 - Accurate Q curve method in long slot
 - Fast Δ decay method in short slot

Todo

- Upgrade Decay method for long slot
 - Compensate for position of Rx coil on Tx coil
 - Additional parameters (resonance wavelength)
 - Influence of component temperature
 - Long slot may require cool down-period
 - Measure R_{on} of MOSFETS

